# Enhanced repulsive Casimir forces between gold and thin magnetodielectric plates

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We calculate repulsive Casimir forces between metallic and magnetic plates and quantitatively probe the magnetic plate's properties as tuning knobs for the repulsion, namely, the plate's thickness and its low-frequency permittivity and permeability. For a thin magnetic plate ( $\leq 10$  nm), we find that repulsion can exist as long as  $\mu(0) \ge \epsilon(0)$ . We also explore the effect of temperature on the repulsion and transition distance between attractive and repulsive interactions. We show how the parameters can be tuned to allow repulsion in submicron separation regimes, making it potentially accessible to known high-resolution measurement techniques using magnetic van der Waals materials.

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## I. INTRODUCTION

In 1948, Casimir theorized that two perfect conducting plates positioned parallel to each other in a vacuum would experience an attractive force arising from the zero-point energy of the vacuum [1], since referred to as the "Casimir force." Lifshitz generalized this work to account for the material's real optical response and thermal fluctuations present at finite temperatures [2]. Dzyaloshinskii, Lifshitz, and Pitaevskii later considered a fluid-filled gap rather than vacuum, discovering the first possibility of switching the interaction between the plates from attraction to repulsion [3]. Repulsion in fluidic systems was later demonstrated in an experiment by Munday *et al.* [4].

Experimentally generating a repulsive Casimir force between two plates separated by less than 1  $\mu$ m in vacuum has eluded the community to date. There have been a few theoretical approaches to potentially overcoming this limitation, which include leveraging nonequilibrium states [5–9], exotic geometries and materials [10–13], and magnetic properties [14–24]. This article focuses on the conditions under which magnetic materials may be used to create repulsive forces and the extent to which currently available materials could be used.

Boyer derived the force between a perfect conducting plate and an infinitely permeable plate [25], which resulted in a purely repulsive force with a magnitude slightly below that which Casimir calculated for the attractive case. Since then, the following question has arisen: How ideal must the materials be to produce repulsion? In real systems, the interaction is not purely repulsive, but rather, it can be attractive at some separations and repulsive at others [16,17,23]. This aspect factors into material choices because more ideal materials, especially magnetic materials, can push the repulsive behavior to shorter separations. Initial generalizations investigated nondispersive media [14]. Although informative for the first steps of real-material implementation, it was noted that dispersion must be included moving forward [26].

With dispersion accounted for, the repulsive component has been shown to be sensitively dependent on the frequency regime over which the magnetodielectric plate's response is mainly magnetic. Further inspection of force behavior, when accounting for frequency dependence [16], showed results similar to those for the nondispersive case, although the repulsion generally occurs at a separation several orders of magnitude below the length scale corresponding to the wavelength of the magnetic resonance frequency. This result first signaled that for repulsion at submicron separations, the magnetic resonance may not necessarily need to occur at visible frequencies.

Despite the results of Ref. [16], in many other systems, the Casimir force at short separations is dictated by the visible-frequency response of the interacting materials. With this in mind, metamaterials have been proposed as a way of producing an artificial magnetic response [15–19]. This property is useful because naturally occurring materials do not have a magnetic response at visible frequencies [26].

Reference [17] probed the connection between the repulsive behavior and the properties of a magnetic metamaterial and found that even a small Drude background in the permittivity of the magnetic metamaterial causes the repulsive component to turn attractive in the micron separation regime but that repulsion can be enhanced by increasing the magnetic anisotropy of the metamaterial. They also found that the magnetic response in the visible regime is not necessarily required to produce a Casimir repulsion at submicron separations, confirming the results in Ref. [16]. However, the authors eventually concluded that measured repulsion (in the relevant  $d = 0.1-1 \,\mu\text{m}$  separation regime) using magnetic metamaterials would be very challenging [18].

Revisiting naturally occurring materials, it has been shown that Casimir repulsion is still theoretically possible in metallic-magnetodielectric systems if the magnetic plate has a significantly strong response and the metallic plate's permittivity at vanishing frequency is described by the

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dissipationless plasma model [20,23]. The latter requirement can be understood when considering that the zero-frequency transverse electric mode provides the sole repulsive contribution to the pressure. In contrast, a dissipative Drude model predicts a vanishing pressure contribution for the transverse electric mode at zero frequency, leaving a purely attractive interaction. While it is an experimental fact that the conductivity of metals such as gold remains finite at low frequencies, which is in agreement with the Drude model, several Casimir experiments are well described by the plasma model, excluding the Drude model with high confidence [27,28]. These results suggest that it is likely that a more complex model, rather than a simple Drude or plasma model, is actually needed to describe the dielectric response of metals for real materials. Thus, metallic-magnetodielectric material systems provide an excellent platform to further experimentally distinguish between the two models as the sign of the Casimir force depends crucially on the modeling as described above. It should be noted that repulsion has also been shown to be present when the metallic plate is replaced with a superconducting material whose permittivity can be described with Lorentz oscillators; however, this effect is caused by its diamagnetic properties, which is a separate, but interesting, system in its own right [29].

For a finite-thickness magnetodielectric plate, its thickness b and permittivity  $\epsilon(\omega)$  and permeability  $\mu(\omega)$  at zero frequency have all been shown to affect the Casimir repulsion [20–23]. The system temperature T has also been shown to enhance repulsion in metamaterial systems through the zero-frequency transverse electric mode [18].

Here, we systematically investigate to what extent each of the preceding parameters can be tuned to enhance the repulsive behavior in a metallic-magnetodielectric system using the largest-magnitude repulsion  $P_{max}$  and separation where the interaction switches from attraction to repulsion  $d_{\rm T}$  as quantitative metrics. This investigation is carried out with the overarching goal of identifying combinations of parameter values that theoretically push this system into an experimentally accessible regime and subsequently allow for the first measurement of a Casimir repulsion in vacuum at submicron separations. Although Casimir-force calculations using ultrathin yttrium iron garnet (YIG) as the magnetodielectric material have shown repulsion in the submicron separation regime [21,23], it is unclear whether the bulk properties of YIG will hold when thinning the material down to just a few nanometers. We therefore reevaluate the parameter space and use our calculations to identify a potential class of alternative materials that could enable repulsion.

We compare our calculations with the force-modulated gradient measurement technique, which is generally performed using an atomic force microscope [30–32]. The theoretical limits to the minimum force and maximum separations over which this technique can work were identified in Ref. [32]. We also consider only Au as the material for the metallic plate, as it is the most common surface used in these measurements and other noble metals generally give similar results.

In addition to the quantitative tuning of already-established connections between the stated system parameters and



FIG. 1. Parallel-plate configuration. The left plate is semiinfinitely thick Au; the right plate is an arbitrary magnetic material. The material permittivities  $\epsilon$  and permeabilities  $\mu$  along with the plate-plate separation d and magnetic-plate thickness b are noted.

repulsive behavior, we show a nontrivial interplay between the plate thickness and  $\mu(0)$ , as well as linearization of the relationship between  $\mu(0)$  and  $\epsilon(0)$  required to generate repulsion  $[\mu(0) \ge \epsilon(0)]$ , previously seen to be nonlinear for infinitely thick plates [20].

The content of this article is partitioned into the following sections: In Sec. II, a generic Au-magnetodielectric system, the underlying theory, and key features in the force behavior are discussed. In Sec. III, we probe the effect of the non-ideality of the magnetodielectric material. In Sec. IV, we look at what relative permeability and thickness regimes are most optimal for repulsion. In Sec. V, the system temperature is considered as an additional tuning knob. Last, in Sec. VI, we draw conclusions as to what combination of parameter values appears to be optimal for the largest repulsion to occur at the smallest separation and identify a class of materials that are excellent candidates for meeting these goals.

# **II. THEORY AND APPLICATION**

We consider a cavity in vacuum formed between a semiinfinite Au plate and a magnetodielectric plate of thickness b, positioned parallel to each other and separated by a distance d(Fig. 1).

#### A. Lifshitz formalism

Within Lifshitz's theoretical framework [2,3], the pressure between the plates can be separated into contributions from the transverse electric (TE) and transverse magnetic (TM) modes described by the following equation:

$$P = P_{\rm TE} + P_{\rm TM},\tag{1}$$

$$P_{j} = -\frac{k_{B}T}{\pi} \sum_{n=0}^{\infty} \int_{0}^{\infty} k \, dk \, \frac{r_{j}^{L} r_{j}^{R,\text{eff}} \, e^{-2\rho_{\text{m}}d}}{1 - r_{j}^{L} r_{j}^{R,\text{eff}} e^{-2\rho_{\text{m}}d}} \rho_{\text{m}} \qquad (2)$$

and  $k_B$  is the Boltzmann constant, T is the system temperature, k is the magnitude of the wave-vector projection onto the surface of the plate(s), and  $r_j^{\text{L}}$  and  $r_j^{\text{R,eff}}$  are the Fresnel reflection coefficients for polarization j at the left (L; Au), and right (R; magnetic material) plate surfaces, respectively.

Taking the finite thickness b of the magnetic plate into account, its effective reflection coefficient is [33]

$$r_{j}^{\text{R,eff}} = \frac{r_{j}^{\text{R}}(1 - e^{-2\rho_{\text{R}}b})}{1 - (r_{j}^{\text{R}})^{2} e^{-2\rho_{\text{R}}b}}.$$
(3)

The Fresnel reflection coefficients for half-spaces have the following forms:

$$r_{\rm TM}^{i} = \frac{\rho_{\rm m}\epsilon_{i} - \rho_{i}}{\rho_{\rm m}\epsilon_{i} + \rho_{i}}, \quad r_{\rm TE}^{i} = \frac{\rho_{\rm m}\mu_{i} - \rho_{i}}{\rho_{\rm m}\mu_{i} + \rho_{i}}, \tag{4}$$

where  $\epsilon_i$  and  $\mu_i$  are the relative permittivity and permeability of media *i* (L: Au, m: vacuum, and R: magnetic material), respectively.  $\rho_i$  is the magnitude of the imaginary component of the wave vector projected onto the *z* axis (normal to the plate surfaces) in media *i* and has the form

$$\rho_i = \sqrt{k^2 + \frac{\epsilon_i \mu_i \xi_n^2}{c^2}},\tag{5}$$

where *c* is the speed of light in vacuum. The summation in Eq. (2) is taken over the Matsubara frequencies  $\xi_n = 2\pi nk_B T/\hbar$ , where  $\hbar$  is the reduced Planck's constant and the prime denotes that the zero-frequency term (n = 0) is multiplied by an additional factor of 1/2.

We describe the relative permittivity of the Au plate by the plasma model in the imaginary frequency domain as

$$\epsilon_{\rm Au}(i\xi) = 1 + \frac{\omega_p^2}{\xi^2},\tag{6}$$

using the plasma frequency  $\omega_p = 9.0 \text{ eV}$ , as in Refs. [34,35]. Au is nonmagnetic, so the permeability of the Au plate is set to  $\mu_{Au}(i\xi) = 1$ .

While we will concentrate on the effect of the magnetic material's permeability, its permittivity cannot be ignored (or simply set to 1) for a realistic material. We have chosen to model the permittivity of the magnetic material after that of bulk YIG. The experimental data for the YIG permittivity along with the upper and lower frequency extrapolations in Ref. [23] are used with Kramers-Kronig relation (7) to calculate  $\epsilon(i\xi)$  for YIG as

$$\epsilon(i\xi) = 1 + \frac{2}{\pi} \int_0^\infty \frac{\omega \operatorname{Im}[\epsilon(\omega)]}{\omega^2 + \xi^2} d\omega.$$
 (7)

As seen in Fig. 2, the permittivities of Au and YIG are infinite and finite, respectively, at  $i\xi = 0$ , as expected from a metal and a dielectric. This choice is reasonable but constrains the scope to magnetic materials with a dielectric character (i.e., materials with a finite permittivity at  $\xi = 0$ ), which is necessary for a more thorough investigation of the other magnetic material parameters.



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FIG. 2. Permittivities for Au and YIG evaluated at imaginary frequencies  $i\xi$ .

Unlike the permittivity, for which some materials could be described with a Drude or plasma background and/or resonances in the visible-frequency regime, the permeability of naturally occurring ferromagnetic materials typically has a response up to only the few-gigahertz frequency regime [36]. It is therefore reasonable for system temperatures near 300 K to treat the magnetic response as quasistatic  $\mu(i\xi = 0) > 1$ and otherwise  $\mu(i\xi > 0) = 1$ . For a more in-depth discussion on this treatment, see Ref. [20]. For most of the work presented here, the value of  $\mu(i\xi = 0)$  will be left arbitrary rather than pinned at the value for YIG [ $\mu(0) = 160$ ], allowing us to explore its dependence on the force.

Special care must be taken for the pressure expressions at  $i\xi = 0$  because divergences and indeterminate values emerge in Eq. (2) during numerical evaluation. In the limit of  $i\xi \rightarrow 0$ , Eqs. (2) and (3) can be rewritten such that  $\rho_{\rm m}$  and  $\rho_{\rm R}$  are both replaced with k and the Fresnel reflection coefficients (4) for the left-plate surface take the forms

$$r_{\text{TE},0}^{\text{L}} = \frac{k - \sqrt{k^2 + \omega_p^2/c^2}}{k + \sqrt{k^2 + \omega_p^2/c^2}}, \quad r_{\text{TM},0}^{\text{L}} = 1$$
(8)

and those for the right-plate surface take the forms

$$r_{\text{TE},0}^{\text{R}} = \frac{\mu(0) - 1}{\mu(0) + 1}, \quad r_{\text{TM},0}^{\text{R}} = \frac{\epsilon(0) - 1}{\epsilon(0) + 1}.$$
 (9)

#### **B.** Typical pressure characteristics

One of the general requirements for generating a repulsive Casimir force in metallic-magnetodielectric systems is that the permittivity of the metallic plate be described by a plasma model at zero frequency. We therefore use Au for the metallic plate because it is a good, nonmagnetic metal and is common in experiments [31,32].

For the purposes of identifying typical features in the force behavior, we consider a cavity in vacuum formed by a semiinfinite Au plate and a 1-µm-thick YIG plate  $[\mu_{\text{YIG}}(0) = 160$ [37] and  $\epsilon_{\text{YIG}}(0) = 4.02$ ] at T = 300 K. The pressure curve and the separated contributions from the TE and TM modes corresponding to  $\xi = 0$  and  $\xi > 0$  normalized by the pressure



FIG. 3. (a) Magnitude of the pressure between a semi-infinite Au plate and a 1-µm-thick YIG plate with the transition separation  $d_{\rm T}$  and maximum repulsion  $P_{\rm max}$  features identified. (b) The corresponding mode contributions from the zero-frequency TE and TM modes (TE<sub> $\xi=0$ </sub> and TM<sub> $\xi=0$ </sub>, respectively) and nonzero-frequency TE and TM modes (TE<sub> $\xi>0$ </sub> and TM<sub> $\xi>0$ </sub>, respectively) normalized by  $P_c$ .

of a perfect conducting cavity in vacuum  $P_c = -\hbar c \pi^2 / 240 d^4$  can be seen in Fig. 3.

Figure 3(a) shows the magnitude of the Casimir pressure experienced by the plates as a function of separation. There are two important features here: the vanishing pressure at  $d \approx 2.26 \,\mu\text{m}$  denoting the switch from attraction to repulsion and the largest-magnitude repulsion occurring at  $d \approx 2.96 \,\mu\text{m}$ . We define the separation where this force switching occurs as the transition separation  $d_{\rm T}$  and the largest-magnitude repulsion as  $P_{\rm max}$ . These two parameters will be used as metrics for the repulsive behavior in the sections below.

Figure 3(b) shows the contributions to the pressure from the TE and TM modes at zero frequency (TE<sub> $\xi=0$ </sub> and TM<sub> $\xi=0$ </sub>, respectively) and the TE and TM modes for all nonzero frequencies (TE<sub> $\xi>0$ </sub> and TM<sub> $\xi>0$ </sub>, respectively), all normalized by  $P_c$ . The modes at nonzero frequencies control the interaction at small separations, and those at zero frequency control the interaction at large separations. Interestingly, we note that for these metallic-magnetodielectric systems, the TE<sub> $\xi=0$ </sub> mode is repulsive.

# III. RELAXED IDEALITY CONDITION FOR MAGNETIC MATERIAL

The initial cavity considered by Boyer consisted of ideal electric and magnetic plates [25]. In real materials, the permittivities and permeabilities are not infinite for all frequencies, nor are the two properties mutually exclusive. Some magnetic



FIG. 4. (a) Relations between the zero-frequency dielectric and magnetic responses of the magnetic material required to maintain  $d_{\rm T} = 6\,\mu{\rm m}$ , calculated for varying thicknesses *b*. Above each line are parameter values that result in repulsion; below are those that result in attraction at  $d_{\rm T} = 6\,\mu{\rm m}$ . (b) Calculations repeated with a single thickness, b = 1 nm, for varying transition separations  $d_{\rm T}$ . The dashed lines correspond to Eq. (17).

materials like Ni and Fe are also electrically conductive, such that repulsion in such systems may not be present. The following question then arises: Is there some upper limit on how electrically conductive the magnetic plate can be in order to maintain repulsion?

To answer this question, for a given value of  $\epsilon(0)$ , we calculate the value of  $\mu(0)$  necessary to keep  $d_T$  pinned at  $6 \mu m$  [Fig. 4(a)]. Because the zero-frequency modes dominate the interaction at separations greater than a few microns, this methods allows us to determine the necessary restrictions on the material properties for repulsion in this surface separation regime.

Previous calculations for two infinitely thick plates showed vertically asymptotic behavior at  $\epsilon(0) \approx 8$ , putting a relatively short ceiling on how conductive the magnetic material could be [20]. However, the situation changes as the magnetic material's thickness is reduced to a few nanometers.

This asymptotic condition relaxes to a linear relation as the thickness is reduced from 10 µm to 1 nm [Fig. 4(a)]. Calculations done at 10 and 1 nm have a slope of  $\approx 1$  in the  $\epsilon(0)$ - $\mu(0)$  plane, suggesting that the condition for repulsion becomes  $\mu(0) \equiv \epsilon(0)$  for very thin films and large separations.

This simple linear relation could be used as a rule of thumb for generating repulsive Casimir forces at large separations, similar to the inequality between the dielectric functions in fluidic systems [4]. As high-resolution experiments are carried out in the submicron separation regime, we repeat the calculations for b = 1 nm with  $d_T = 1 \mu m$ , 800 nm, 600 nm, and 400 nm. As shown in Fig. 4(b), the linearity persists, yet the slope increases with decreasing  $d_T$ . There is also a constant positive shift in  $\mu(0)$  as the repulsive, zero-frequency TE mode has to compensate for the attractive, nonzero-frequency modes that become dominant in the submicron separation regime.

To understand the behavior of the numerical curves in Fig. 4(b), we apply several approximations to Lifshitz's formula (1) to obtain an analytical expression for  $\epsilon(0)$  in terms of  $\mu(0)$  which is in agreement with the calculations. For each curve, the total pressure contribution for all nonzero Matsubara frequencies is constant. In the following, we thus apply approximations to only the zero-frequency pressure contribution and keep the contribution of the nonzero Matsubara frequencies exact.

Notice that while the magnetic slab for the data in Fig. 4(b) is very thin (b = 1 nm), the values of the permittivity  $\epsilon(0)$  and permeability  $\mu(0)$  are quite high. Thus, there is competition between physical thickness *b* and optical thickness for the effective reflection coefficient on the thin magnetic film. The optical thickness is related to the reflection coefficients of the corresponding half slab  $r_{j,0}^{R}$ . It is high if  $|r_{j,0}^{R}| \approx 1$  and low if  $r_{j}^{R} \approx 0$ .

The competition between physical and optical thicknesses becomes evident when examining the limiting behaviors of small physical thickness and large optical thickness separately. On the one hand, keeping  $r_{j,0}^{R}$  fixed and expanding Eq. (3) for small *b*, we obtain  $r_{j,0}^{R,eff} \approx 2kb r_{j,0}^{R}/[1 - (r_{j,0}^{R})^2]$ . On the other hand, if we keep *b* fixed and expand Eq. (3) around  $r_{j,0}^{R} = \pm 1$ , where the upper sign corresponds to j =TM and the lower one corresponds to j = TE, we find  $r_{j,0}^{R,eff} =$  $\pm 1$ . What happens if the physical thickness is small and the optical thickness is large at the same time, as is the case for the data in Fig. 4(b)? The competition between physical and optical thicknesses can be captured by introducing an effective thickness of the slab by

$$b_{j,\text{eff}} = 2b \frac{r_{j,0}^{\text{R}}}{1 - \left(r_{j,0}^{\text{R}}\right)^2}.$$
 (10)

Notice that for transparent slabs  $[\epsilon(0), \mu(0) = 1]$  the effective thickness becomes zero, as it should. For  $\epsilon(0), \mu(0) \gg 1$ , the effective thickness becomes  $b_{\text{TM,eff}} \approx b\epsilon(0)/2$  and  $b_{\text{TE,eff}} \approx b\mu(0)/2$  for the two polarizations, respectively. We will make use of this approximation for our final result in Eq. (17).

If we now keep  $b_{j,\text{eff}}$  fixed and expand Eq. (3) around  $|r_{j,0}^{\text{R}}| = 1$  [which is valid for the large values of  $\mu(0)$  and  $\epsilon(0)$ 

considered here], we obtain, to leading order,

$$r_{j,0}^{\text{R,eff}} \approx \frac{kb_{j,\text{eff}}}{kb_{j,\text{eff}}+1}.$$
 (11)

Indeed, this expression agrees with the limiting behaviors for small physical thickness and large optical thickness discussed above.

As a next step, we approximate the reflection coefficients on the left plate for TE polarization given in (8). As gold has a relatively high plasma frequency, we can expand the reflection coefficient for  $\omega_p/c \ll k$  and find

$$r_{\text{TE},0}^{\text{L}} \approx -1 + 2\frac{ck}{\omega_p} - 2\frac{c^2k^2}{\omega_p^2} + O\left(\frac{c^3k^3}{\omega_p^3}\right).$$
 (12)

The expansion up to second order in  $ck/\omega_p$  will be accurate for the separations considered here.

With approximations (11) and (12) we can now find an approximation for the pressure contributions at zero frequency. Introducing the expansion coefficient  $\beta_j = b_{j,\text{eff}}/d$ , we Taylor expand the pressure contributions up to second order around  $\beta_j = 0$  and find

$$P_{\rm TE} \approx \frac{k_B T}{2\pi d^3} [\gamma_1 \beta_{\rm TE} - \gamma_2 \beta_{\rm TE}^2 + O(\beta_{\rm TE}^3)],$$
  
$$P_{\rm TM} \approx -\frac{k_B T}{2\pi d^3} \left(\frac{3}{8} \beta_{\rm TM} - \frac{99}{128} \beta_{\rm TM}^2 + O(\beta_{\rm TM}^3)\right), \quad (13)$$

with the positive coefficients

$$\gamma_1 = \frac{3}{8}(1 - 4\alpha + 10\alpha^2),$$
  

$$\gamma_2 = \frac{99}{128} \left(1 - \frac{495}{99}\alpha + 15\alpha^2\right),$$
(14)

and  $\alpha = c/(d\omega_p)$ .

The Taylor expansions (13) are accurate when  $\beta_j \ll 1$ . Notice that this requirement is actually not quite met for the parameter range considered in Fig. 4(b), as the expansion coefficients take values in the range  $0 \leq \beta_{\text{TE}} \leq 0.25$  and  $0 \leq \beta_{\text{TM}} \leq 0.125$ . In fact, expressions (13) yield a rather poor approximation of the numerical curves. A better approximation can be found using a Padé approximant. We find

$$P_{\rm TE} \approx \frac{k_B T}{2\pi d^3} \frac{\gamma_1^2 \beta_{\rm TE}}{\gamma_2 \beta_{\rm TE} + \gamma_1},$$
  
$$P_{\rm TM} \approx -\frac{k_B T}{2\pi d^3} \frac{6\beta_{\rm TM}}{33\beta_{\rm TM} + 16}.$$
 (15)

The coefficients of the Padé approximants are found by expanding the rational functions around  $\beta_j = 0$  and comparing the coefficients with the ones from the respective Taylor expansion (13).

Finally, we can leverage the zero-pressure condition that holds true for all calculations included in Fig. 4,

$$P_{\rm TE}^0 + P_{\rm TM}^0 + P^{\xi > 0} = 0, \tag{16}$$

along with Eqs. (15) to derive the relation between  $\epsilon(0)$  and  $\mu(0)$ :

$$\mu(0) \approx \frac{2d}{b} \frac{A\epsilon(0) + B}{C\epsilon(0) + D},\tag{17}$$



FIG. 5. (a) Maximum repulsion  $P_{\text{max}}$  and (b) transition separation  $d_{\text{T}}$  as a function of the permeability of the magnetic plate  $\mu(0)$  for a few plate thicknesses *b*.

with  $A = (6 + 33\delta)\gamma_1 b/(2d)$ ,  $B = 16\gamma_1\delta$ ,  $C = [33\gamma_1^2 - (6 + 33\delta)\gamma_2]b/(2d)$ ,  $D = 16(\gamma_1^2 - \gamma_2\delta)$ , and  $\delta = -2\pi d^3 P^{\xi>0}/(k_BT)$ . The results corresponding to Eq. (17) are shown by the dashed lines in Fig. 4(b). They agree well with the numerical data, validating the linear behavior of the results. The discrepancy between the numerical and analytical results becomes stronger as  $d_T$  decreases and is thus most pronounced for the blue curves with  $d_T = 400$  nm. This is expected because that curve corresponds to the largest values of  $\beta_j$ . The accuracy of the analytical results can be improved by calculating a Padé approximant of higher order.

It should be noted that the optical properties of bulk materials likely break down at  $\sim 1$  nm thicknesses; however, we continue to characterize the magnetic plate with the permittivity of bulk YIG, as the purpose of this work is to better understand the connections between system parameters and repulsion so that a class of magnetic material candidates can be identified. Similarly, we exclude anisotropic features and nonlocal effects that will likely emerge in the optical response for thin plates, leaving them for future study.

### IV. TUNING PLATE THICKNESS AND PERMEABILITY

Both the zero-frequency permeability  $\mu(0)$  and the plate thickness *b* are known to affect the repulsion [20,21,23]. Here, we use the transition separation  $d_T$  and maximum repulsion  $P_{\text{max}}$  [Fig. 3(a)] as metrics to quantitatively explore their effect and the interplay between these two parameters. In Figs. 5(a) and 5(b), there is a monotonic decrease in  $d_T$  and an increase in  $P_{\text{max}}$  as  $\mu(0)$  increases. The same relation is seen with a decreasing thickness *b*. Our results suggest one should use a



FIG. 6. Maximum repulsion  $P_{\text{max}}$  calculated as a function of magnetic plate thickness *b* for a few permeability values  $\mu(0)$ . The black crosses mark the maxima for each curve.

material with a large permeability and one that is as thin as possible.

Although  $P_{\text{max}}$  appears monotonic with  $\mu(0)$ , it does not asymptotically approach  $\infty$  as  $b \rightarrow 0$ . To probe this effect, we keep  $\mu(0)$  fixed and vary b (Fig. 6).  $P_{\text{max}}$  increases as b decreases, eventually reaching a peak, beyond which  $P_{\text{max}}$ falls towards zero. Further, the peak repulsive pressure shifts to lower thicknesses, and the descent of  $P_{\text{max}}$  towards zero becomes more dramatic for larger values of  $\mu(0)$ . This result shows that there is such a thing as "too thin," and the critical thickness where  $P_{\text{max}}$  reaches its peak largely depends on  $\mu(0)$ .

As expected,  $P_{\text{max}}$  approaches zero as  $b \rightarrow 0$  because if the plate thickness goes to zero, the cavity disappears. The initial increase in  $P_{\text{max}}$  as *b* is reduced from bulk thickness can be understood from the different scalings of the  $\text{TE}_{\xi\rightarrow 0}$  and  $\text{TM}_{\xi\rightarrow 0}$  pressure contributions with the thickness *b*. The attractive  $\text{TM}_{\xi\rightarrow 0}$  mode diminishes more quickly than the repulsive  $\text{TE}_{\xi\rightarrow 0}$  mode with decreasing *b*, leaving an apparent enhancement of the overall repulsion. This phenomenon is described within the context of diamagnetic-ferromagnetic material systems [21], and here, the same argument can be made.

### V. THERMAL EFFECTS

Beyond the properties of the magnetodielectric material, the system temperature can also be used to enhance repulsion. This phenomenon was initially suspected when considering that the temperature can be used to modulate the attraction between two nonmagnetic metals at large separations through the zero-frequency modes [38]. Unlike cavities formed by nonmagnetic metal plates, where an enhanced attraction is seen due to the zero-frequency modes providing attractive contributions, the zero-frequency TE mode in the metallicmagnetodielectric system provides a repulsive contribution and one that dies more slowly with increasing separation than the corresponding attractive TM mode. This connection was confirmed within the context of metallic-metamaterial systems [18].

Here, we investigate how much we can decrease the transition separation  $d_{\rm T}$  using experimentally reasonable



FIG. 7. Pressure between Au and a 1-nm-thick magnetic plate calculated as a function of separation with (a)  $\mu(0) = 20$  and (b)  $\mu(0) = 160$ . Calculations are performed for temperatures of 300, 305, and 310 K.

increases in temperature. The pressure curves in Fig. 7(a) were calculated using  $\mu(0) = 20$  and  $\epsilon_{\rm R}(i\xi) = \epsilon_{\rm YIG}(i\xi)$ . Imposing a modest temperature increase from 300 to 310 K results in  $\Delta d_{\rm T} = -36.4$  nm. In Fig. 7(b), pressure curves were again calculated at 300, 305, and 310 K, but this time with  $\mu(0) = 160$ . With  $d_{\rm T}$  now being much smaller at ~240 nm, the shift in the transition separation driven by the 10 K temperature increase is much smaller at  $\Delta d_{\rm T} = -5.6$  nm.

From these results, although the gains might be modest, it appears that higher temperatures would be beneficial for pushing the repulsion to lower separations. One must be careful, however, not to increase the temperature above the Curie point of the magnetodielectric where the thermal excitations will destroy the magnetic ordering. Higher temperatures will also increase the thermal measurement noise [32].

### **VI. CONCLUSIONS**

We have shown how three parameters related to the magnetic plate  $[\epsilon(0), \mu(0)]$ , and b] and the system temperature T can be leveraged to enhance and modulate the repulsion in metallic-magnetodielectric plate systems. Our results concerning the ideality of the magnetic material are consistent with previous work [20]; however, we show that when the thickness b is decreased to only a few nanometers, the required relation between  $\mu(0)$  and  $\epsilon(0)$  for generating repulsion at large separations is  $\mu(0) = \epsilon(0)$  and stays linear well into the submicron separation regime. Further, a large magnetic permeability [preferably  $\mu(0) > 1000$ ] and a small thickness  $(b \sim 1 \text{ nm})$  can drive repulsion on a millipascal scale within a few-hundred-nanometer separation regime, although there is a lower limit on how thin the material can be before the pressure decreases. Last, high temperatures (but below the Curie point) are optimal because they can boost the repulsive zero-frequency TE mode contribution.

From this investigation, we identify magnetic van der Waals materials [39,40] as excellent candidates for these systems, given their nanometer-scale and even subnanometerscale thicknesses. These materials could potentially be used to generate repulsive Casimir forces in vacuum (or air) using current techniques [30,32] and even levitated above a Au sample, similar to the experiment seen in Ref. [41] using a fluid. Beyond the potential measurement of repulsive forces in air, subsequent measurements could provide additional experimental evidence for the appropriateness of plasma or Drude models when discussing Casimir forces (see, e.g., Refs. [42–44]).

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